A Practical Guide to 'Free Energy' Devices

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This patent application shows a very neat, self-powered electrical generator with a theoretical output of anything up to a COP of 59 when using cadmium selenide. The discussion of the theoretical aspects of the design includes a large amount of historical information and it covers the origin of the "law" of Conservation of Energy which, in spite of being incorrect, has been for decades, a major obstacle to the scientific development of free-energy devices.

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SELF-SUSTAINING ELECTRIC POWER GENERATOR UTILISING ELECTRONS **OF LOW INERTIAL MASS TO MAGNIFY INDUCTIVE ENERGY**

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ABSTRACT

Electrical oscillations in a metallic "sending coil" radiate inductive photons toward one or more "energymagnifying coils" comprised of a photoconductor or doped semiconductor coating a metallic conductor, or comprised of a superconductor. Electrons of low inertial mass in the energy-magnifying coil(s) receive from the sending coil, a transverse force having no in-line backforce, which exempts this force from the energyconservation rule. The low-mass electrons in the energy-magnifying coil(s) receive increased acceleration proportional to normal electron mass divided by the lesser mass. Secondarily radiated inductive-photon energy is magnified proportionally to the electrons' greater acceleration, squared, e.g., the inductive-energymagnification factor of CdSe photoelectrons with 0.13 x normal electron mass is 59 times. Magnified inductive-photon energy from the energy-magnifying coil(s) induces oscillating electric energy in one or more metallic "output coil(s)". The electric energy output exceeds the energy input if more of the magnified photon induction energy is directed toward the output coil(s) than is directed as a counter force to the sending coil. After an external energy source initiates the oscillations, feedback from the generated surplus energy makes the device a self-sustaining generator of electric power for useful purposes.

CROSS REFERENCE TO RELATED APPLICATION

This application corresponds to, and claims the benefit under 35 U.S.C. 119(e), of U.S. provisional application No. 60/697,729, filed on 8th July 2005, incorporated herein by reference in its entirety.

FIELD

This disclosure introduces a technical field in which practical electrical energy is created in accordance with the overlooked exception to the energy-conservation rule that Herman von Helmholtz described in his 1847 doctrine on energy conservation: "If . . . bodies possess forces which depend upon time and velocity, or which act in directions other than lines which unite each pair of material points, . . . then combinations of such bodies are possible in which force may be either lost or gained as infinitum". A transverse inductive force qualifies for Helmholtz's ad infinitum rule, but this force is not sufficient of itself to cause a greater energy output than input when applied to electrons of normal mass due to their unique charge-to-mass ratio. However, the increased acceleration of conduction electrons of less-then-normal inertial mass, as occurs in photoconductors, doped semiconductors, and superconductors, is proportional to the normal electron mass divided by the low electron mass, and the magnification of harnessable inductive energy is proportional to the square of the greater relative acceleration.

BACKGROUND

Magnetic force also satisfies Helmholtz's exemption to the energy-conservation rule because magnetic force is transverse to the force that causes it, and magnetic force is determined by the "relative velocity" (i.e. perpendicular to the connecting line) between electric charges. Magnification of magnetic force and energy was demonstrated by E. Leimer (1915) in the coil of a speaker phone and in the coil of a galvanometer when he irradiated a radio antenna-wire with radium. A 10 milligram, linear radium source produced a measured 2.6 fold increase in electrical current in the antenna wire in comparing inaudible radio reception without radium to audible reception with radium. This represented a $(2.6)^2 = 7$ times increase in electrical energy flowing through the respective wire coils. The possibility of this enhanced reception being attributed to a person's body holding the unit of radium to the wire was eliminated by Leimer's additional observation that whenever the orientation of the small radium unit was changed to approximately 30 degrees relative to the wire, the energy enhancement ceased.

Applicant has deduced that Leimer's energy magnification was most likely due to low-mass electrons that were liberated and made conductive in the antenna by alpha radiation, which allowed these special electrons to be given a greater than normal acceleration by the received radio broadcast photons. Applicant has further deduced that such low-mass electrons must have originated in a thin-film coating of cupric oxide (CuO) on the antenna wire. CuO is a dull black polycrystalline semiconducting compound that develops in situ on copper and bronze wire in the course of annealing the wire in the presence of air. Such CuO coatings have been observed by Applicant on historical laboratory wire at the Science Museum at oxford University, U.K. and on copper house wire of that era in the U.S., indicating that CuO coatings were commonplace. In later years, annealing has taken place under conditions that prevent most oxidation. This is followed by acid treatment to remove any remaining oxides, leaving shiny wire.

The same year that the English translation of Leimer's paper appeared in *Scientific American*, 16-year old Alfred M. Hubbard of Seattle, Washington, reportedly invented a fuelless generator, which he later admitted, employed radium. Applicant interprets this as implying that Leimer's energy-magnification was utilised by Hubbard with feedback to make it self-sustaining. Three years later, Hubbard publicly demonstrated a relatively advanced fuelless generator that illuminated a 20-watt incandescent bulb (Anon. 1919a). A reputable physics professor from Seattle College, who was intimately familiar with Hubbard's device (but not at liberty to disclose its construction details), vouched for the integrity of the fuelless generator and declared that it was not a storage device, but he did not know why it worked (Anon. 1919b). Because Hubbard initially had no financial means of his own, it is likely that the professor had provided Hubbard with the use of the expensive radium initially and thereby witnessed the inventing process in his own laboratory.

Newspaper photos (Anon. 1920a) of a more impressive demonstration of Hubbard's fuelless generator, show a device described as 14 inches (36 cm) long and 11 inches (28 cm) in diameter, connected by four heavy electrical cables to a 35 horsepower (26 kW) electric motor. The motor reportedly propelled an 18-foot open launch around a like at a speed of 8 to 10 knots (Anon. 1920b). The event was witnessed by a cautious news reporter who claims to have checked thoroughly for any wires that might have been connected to hidden batteries, by lifting the device and motor from the boat. Radioactive-decay energy can be eliminated as the main power source because about 10⁸ times more radium than the entire world's supply would have been needed to equal Hubbard's reported electric energy output of 330 amperes and 124 volts.

Lester J. Hendershott of Pittsburgh, Pa., reportedly demonstrated a fuelless generator in 1928 that was claimed by Hubbard to be a copy of his own device (1928h). The president of Stout Air services, William B. Stout, who also designed the Ford Trimotor aeroplane, reported (1928b): "The demonstration was very impressive. It was actually uncanny.... The small model appeared to operate exactly as Hendershot explained it did". Also reportedly attesting to the operability of Hendershott's fuelless generator were Colonel Charles A. Lindbergh and Major Thomas Lanphier of the U.S. Air Corps (1928a, et seq.), and Lanphier's troops reportedly assembled a working model of his device.

To the Applicant's best knowledge, the only depiction that was made public of the interior components of any of these reported generators consists of a sketchy drawing (Bermann 1928h) of Hubbard's apparatus similar in size to the device shown in his 1919 demonstration. It depicts a complex set of parallel coils measuring 6 inches (15 cm) in length and 4.5 inches (11.4 cm) in overall diameter. Four leads of insulated wire, with the insulation peeled back, are shown coming out of the end of the device. What those four wires were connected to internally was not shown. Hubbard's description of the internal arrangement of coils in the device generally matches the drawing (Anon. 1920a): "It is made up of a group of eight electromagnets, each with primary and secondary windings of copper wire, which are arranged around a large steel core.

The core likewise has a single winding. About the entire group of cells is a secondary winding". Nothing was reported or depicted about how components functioned with each other, or how much radium was used and where the radium was positioned. The only connectors visible on the drawing were between the outer windings of the eight electromagnet coils. These connectors show that the direction of the windings alternated between clockwise and counterclockwise on adjacent coils, so that the polarity of each electromagnet would have been opposite to that of it's adjacent neighbours.

If the Hubbard and Hendershot devices actually operated as reported, they apparently never attained acceptance or commercial success. Assuming the devices actually worked, their lack of success may have been largely financially or supply based, or both, compounded with scepticism from believers in the energy-conservation doctrine. How much radium was employed by Hubbard in his larger generator can only be guessed at, but assuming a typical laboratory radium needle containing 10 milligrams of radium was used, that amount would have cost \$900 in 1920, dropping to \$500 in 1929. That much radium in a fuelless generator would have cost as much as an inexpensive automobile in the 1920s. Possibly much more radium was used than 10 milligrams.

In 1922, when the Radium Company of America of Pittsburgh, Pa., reportedly discontinued its work with Hubbard on his invention (1928h), the entire world's supply of radium was only about 250 grams. With the extreme assumption that only 1 milligram of radium was needed per generator, less than 10% of a single year's production of autos in the US in the mid-1920s could have been supplied with such generators. Apparently Hendershott had tried to revive the technology by showing that the fuelless generator could extend the range of air flight indefinitely, but his technology never attracted a sponsor from any private, public or philanthropic entity.

U.S. Pat. No. 4,835,433 to Brown, superficially resembles the drawing of Hubbard's device. Brown's device appears to have the same number and essentially the same general arrangement of wire coils as Hubbard's generator, as nearly as can be understood from the newspaper articles depicting that device. Apparently, no information concerning either the Hubbard or Hendershot devices was considered during the prosecution of the '433 patent. Brown discusses the conversion of energy of radioactive decay products, principally alpha emissions, to electrical energy by amplifying electrical oscillations in a high-Q L-C circuit irradiated by radioactive materials. "During the absorption process, each alpha particle will collide with one or more atoms in the conductor, knocking electrons from their orbits and imparting some kinetic energy to the electrons in the conductor, thereby increasing its conductivity". (Col. 3, Line 68 to Col. 4, line 5). No claim was made by Brown, that the device employed a semiconductor or photoconductor that could have provided low-mass electrons for energy magnification.

Brown claimed an output of 23 amps at 400 volts, which is vastly greater than all the decay energy represented by his reported radioactive content of 1 milligram of radium that was surrounded by weakly radioactive uranium rods and thorium powder. Powered thorium is highly pyrophoric, so it is typically sealed in a nitrogen atmosphere to prevent spontaneous combustion. In his device, Brown reportedly confined the thorium in cardboard without any mention of sealing out air. This condition would have invited a meltdown that could have been interpreted as massive out-of-control electrical production.

To the best of the Applicant's knowledge, no person other than the Applicant has ever indicated that the presence of cupric oxide on their wires could have provided energy magnification. If Hubbard's device actually did work, certain characteristics of its design are unexplainable by the Applicant, namely the use of four rather than two large electrical cables to connect his device to an electrical motor, and the use of alternating polarity instead of single-direction polarity in the orientation of the multiple coils surrounding a central coil. Applicant therefore believes that the specification herein sets forth original configurations of electrical-energy generators that have no known precedent.

SUMMARY

To address the needs for electrical generators which are capable of self-generating substantial amounts of electrical power in various environments, and which are portable as well as stationary, apparatus and methods are provided for magnifying an electrical input, and (with feedback) for generating usable electrical power indefinitely without fuel or other external energy source, except for starting. The apparatus utilises electrons of low effective mass, which receive greater acceleration than normal electrons in an amount that is inversely proportional to the effective mass. Applicant has determined that effective mass is the same as the electron's true inertial mass. The photon energy that is radiated when an electron is accelerated is proportional to the square of the acceleration, so the increase in radiated photon energy from an accelerated low-mass electron over the energy from a normal electron is equal to the inverse square of the effective mass, e.g. the calculated energy magnification provided by photoconducting electrons in cadmium selenide, with an electron effective mass of 0.13, is 59 times. The use of a transverse force, that lacks a direct back-

force, to accelerate low-mass electrons in an oscillating manner, circumvents any equal-and-opposite force that would invoke the application of the energy-conservation law of kinetics and thermodynamics.

The various embodiments of the apparatus, which are configured either to continuously magnify an input of oscillating electric energy, or to serve as a self-sustaining electric generator, employ three principal components:

At least one sending coil

At least one energy-magnification coil, comprising a material that produces , in a "condition" low-mass electrons, and

At least one output coil.

It is desirable that the apparatus also includes a means for establishing the condition with respect to the energy-magnifying coil(s). Except where otherwise indicated in the remainder of this text, where the number of coils of a particular type is referred to in the singular, it will be understood that a plurality of coils of the respective type can alternatively be utilised.

Electrical oscillation in the sending coil, which is comprised of a metallic conductor, causes radiation of inductive photons from the sending coil. The energy-magnifying coil is situated in a position relative to the sending coil so as to receive inductive photons from the sending coil. The inductive photons radiating from electrical oscillations in the sending coil, convey a transverse force to the low-mass electrons in the energy-magnification coil with no back-force on the sending coil. The greater-than-normal accelerations which are produced in the low-mass electrons of the energy-magnifying coil, produce greater irradiation energy of inductive photons than normal.

The output coil is positioned so as to receive the magnified inductive-photon energy from the energymagnifying coil. The inductive-photon energy received by the output coil, which is comprised of a metallic conductor, is converted into an oscillating electrical current of normal electrons. In order for the electrical output to exceed the electrical input, the output coil is situated in such a manner that it receives more of the magnified inductive-photon energy than that which is directed back against the sending coil to act as a backforce. This "energy leverage" causes the electrical energy output to exceed the electrical energy input.

By way of example, the energy-magnifying coil can comprise a superconducting material, wherein the "condition" is a temperature (e.g. a cryogenic temperature) at which the superconducting material exhibits superconducting behaviour characterised by production of low-mass electrons.

By way of another example, the energy-magnifying coil can comprise a photoconductive material, wherein the "condition" is a situation in which the photoconductive material is illuminated by a wavelength of photon radiation sufficient to cause the photoconductive material of the energy-magnifying coil to produce conduction electrons having low effective mass. In this latter example, the means for establishing the condition can comprise a photoconductor exciter (e.g. one or more LEDs) situated and configured to illuminate the photoconductive material of the energy-magnifying coil with the wavelength of photon radiation.

By way of yet another example, the "condition" is the presence of a particular dopant in a semiconductor that provides a low-mass electron as a charge carrier. Also, by way of example, the energy-magnifying coil can comprise a semiconductive element or compound that has been doped with a particular element or compound that makes it conductive of low-mass electrons without illumination by photon radiation other than by ambient photons.

Various apparatus embodiments comprise different respective numbers and arrangements of the principal components. The various embodiments additionally can comprise one or more of circuitry, energisers, shielding and other components to fulfill the object of providing a self-sustaining source of electrical power for useful purposes.

Also provided, are methods for generating an electrical current. In an embodiment of such a method, a first coil is energised with an electrical oscillation sufficient to cause the first coil to radiate inductive photons. At least some of the radiated inductive photons from the first coil are received by a second coil, called "the energy-magnifying coil", comprising a material that produces low-mass electrons. The received inductive photons impart respective transverse forces to the low-mass electrons that cause the low-mass electrons to experience accelerations in the material which are greater than accelerations that otherwise would be experienced by normal free electrons experiencing the transverse forces.

Conduction of the accelerated low-mass electrons in the second coil, causes the second coil to produce a magnified inductive force. The magnified inductive force is received by a third coil which causes the third coil to produce an oscillating electrical output of normal conduction electrons which has greater energy than

the initial oscillation. A portion of the oscillating electrical output is directed as feed-back from the third coil to the sending coil, so as to provide the electrical oscillation to the sending coil. This portion of the oscillating electrical current directed to the sending coil, desirably is sufficient to cause self-sustaining generation of inductive photons by the first coil without the need for any external energy source. The surplus oscillating electrical output from the third coil can be directed to a work loop.

The method can further comprise the step of starting the energisation of the first coil to commence generation of the oscillating electrical output. This "starting" step can comprise momentarily exposing the first coil to an external oscillating inductive force or for example, to an external magnetic force which initiates an electrical pulse.

The foregoing and additional features and advantages of the invention will be more readily apparent from the following detailed description, which proceeds with reference to the accompanying drawings.

BRIEF DESCRIPTION OF THE DRAWINGS



Fig.1A is a perspective view schematically depicting a sending coil in relationship to an energy-magnifying coil such that inductive photons from the sending coil, propagate to the energy-magnifying coil.



Fig.1B is a schematic end-view of the sending coil and energy-magnifying coil of **Fig.1A**, further depicting radiation of inductive photons from the sending coil and the respective directions of electron flow in the coils.



Fig.1C is a schematic end-view of the sending coil and energy-magnifying coil of **Fig.1A**, further depicting the production of inwardly-radiating and outwardly-radiating magnified inductive photons from the energy-magnifying coil.



Fig.2A is a perspective view schematically showing an internal output coil, coaxially nested inside the energy-magnifying coil to allow efficient induction of the internal output coil by the energy-magnifying coil, wherein the induction current established in the internal output coil is used to power a load connected across the internal output coil.



Fig.2B is a schematic end-view of the coils shown in **Fig.2A**, further depicting the greater amount of magnified inductive-photon radiation that is received by the external output coil in comparison to the lesser amount that is directed toward the sending coil to act as a back-force.



Fig.3 is an electrical schematic diagram of a representative embodiment of a generating apparatus.



Fig.4 is a schematic end-view of a representative embodiment, comprising a centrally disposed sending coil surrounded by six energy-magnifying coils, each having and axis which is substantially parallel to the axis of the sending coil. A respective internal output coil is coaxially nested inside each energy-magnifying coil, and the energy-magnifying coils are arranged so as to capture substantially all the inductive photons radiating from the sending coil.



Fig.5 is a schematic end-view of the embodiment of **Fig.4**, further including an external output coil situated coaxially with the sending coil and configured to surround all six energy-magnifying coils so as to capture outwardly-radiating inductive photons from the energy-magnifying coils. Also depicted is the greater amount of magnified inductive-photon radiation that is received by the internal output coils and the external output coil in comparison to the lesser amount of inductive-photon radiation that is directed towards the sending coil to act as a back-force. Also shown are the arrays of LEDs used for exciting the energy-magnifying coils to become photoconductive.



Fig.6 is a perspective view of the embodiment of Fig.4 and Fig.5 but further depicting respective inter-coil connections for the energy-magnifying and internal output coils, as well as respective leads for the sending coil, internal output coils and external output coil.



Fig.7 is a head-end view schematically depicting exemplary current-flow directions in the sending coil, energy-magnifying coils, internal output coils, and external output coils, as well as in the various inter-coil connections of the embodiment of **Fig.4**.



Fig.8 is a schematic end-view showing an embodiment of the manner in which inter-coil connections can be made between adjacent energy-magnifying coils.



Fig.9A is a schematic end-view depicting the coil configuration of an embodiment in which a sending coil and an internal output coil are nested inside an energy-magnifying coil, which in turn is nested inside an exterior output coil. A metallic separator, having a substantially parabolic shape, and being situated between the sending coil and the internal output coil, reflects some of the otherwise unused inductive-photon radiation to maximise the effective radiation received by the energy-magnifying coil. Also, the metallic shield prevents the internal output coil from receiving radiation sent from the sending coil.



Fig.9B is a schematic end-view of the coil configuration of **Fig.9A**, further depicting the metallic separator acting as a shield to restrict the back-force radiation reaching the sending coil while allowing the internal output coil to receive a substantial portion of the magnified radiation from the energy-magnifying coil. Also depicted is the greater amount of magnified inductive-photon radiation that is received by the internal output coil and the external output coil in comparison to the lesser amount that is received by the sending coil to act as a back-force.



Fig10A is a schematic end-view depicting the coil configuration of yet another embodiment that is similar in some respects to the embodiment of **Fig.4**, but also including respective ferromagnetic cores inside the sending coil and internal output coils. Also depicted is a metallic shield surrounding the entire apparatus.



Fig.10B is a schematic end-view of a sending coil of yet another embodiment in which a ferromagnetic sleeve is disposed coaxially around the sending coil.

DETAILED DESCRIPTION

General Technical Considerations

An understanding of how "infinite energy" mistakenly came to be rejected by the scientific community, clarifies the basis of this invention. The electrodynamic function described in the embodiments described below, conforms to Helmholtz's alternate energy rule, which states that a force which is not in line with it's causative force "may be lost or gained ad infinitum". This rule was included in "Uber die Erhaltung der Kraft" ("On the Conservation of Force") that Hermann Helmholtz delivered to the Physical Society of Berlin in 1847. But, Helmholtz mistakenly believed that "all actions in nature are reducible to forces of attraction and repulsion, the intensity of the forces depending solely upon the distances between the points involved so it is impossible to obtain an unlimited amount of force capable of doing work as the result of any combination whatsoever of natural objects".

Helmholtz refused to accept the idea that magnetic energy qualifies for ad infinitum status despite the fact that Ampere's (1820) magnetic force on parallel straight conductors is obviously transverse to the direction of the electric currents rather than being in line with the currents. He omitted mention that the magnetic force in Ampere's (1825) important invention, the solenoidal electromagnet, is caused by currents in the loops of his coils, which are transverse to the direction of magnetic force. Also, he failed to mention that Ampere considered the magnetic force of a permanent magnet to be caused by minute transverse circular currents, which are now recognised as electrons that spin and orbit transversely.

Helmholtz, who was educated as a military medical doctor without any formal study of physics, relied instead on an obsolete metaphysical explanation of magnetic force: "Magnetic attraction may be deduced completely

from the assumption of two fluids which attract or repel in the inverse ratio of the square of their distance....It is known that the external effects of a magnet can always be represented by a certain distribution of the magnetic fluids on its surface". Without departing from this belief in magnetic fluids, Helmholtz cited Wilhelm Weber's (1846) similarly wrong interpretation that magnetic and inductive forces are directed in the same line as that between the moving electric charges which cause the forces.

Weber had thought that he could unify Coulombic, magnetic, and inductive forces in a single, simple equation, but Weber's flawed magnetic-force term leads to the absurd conclusion that a steady current in a straight wire induces a steady electric current in a parallel wire. Also, a changing current does not induce an electromotive force in line with the current, as Weber's equation showed. The induced force is offset instead, which becomes more apparent the further that two nested, coaxial coils are separated. What appears to be a directly opposing back-force is actually a reciprocal inductive force.

Helmholtz's assertion that the total sum of the energy in the universe is a fixed amount that is immutable in quantity from eternity to eternity appealed to his young friends. But, the elder scientists of the Physical Society of Berlin declared his paper to be "fantastical speculation" and a "hazardous leap into very speculative metaphysics", so it was rejected for publication in Annalen der Physik. Rather than accept this rejection constructively, Helmholtz found a printer willing to help him self-publish his work. Helmholtz headed the publication with a statement that his paper had been read before the Society, but he disingenuously withheld mention of its outright rejection. Unwary readers have since received the wrong impression that his universal energy-conservation rule had received the Society's endorsement rather than its censure.

Helmholtz (1862, 1863) publicised his concept thus: "We have been led up to a universal natural law, which ... expresses a perfectly general and particularly characteristic property of all natural forces, and which ... is to be placed by the side of the laws of the unalterability of mass and the unalterability of the chemical elements". Helmholtz (1881) declared that any force that did not conserve energy would be "in contradiction to Newton's axiom, which established the equality of action and reaction for all natural forces" (sic). With this deceitful misrepresentation of Newton's strictly mechanical principle, Helmholtz had craftily succeeded in commuting the profound respect for Newton's laws to his unscientific doctrine. Subsequently, the Grand Cross was conferred on Helmholtz by the kings of Sweden and Italy and the President of the French Republic, and he was welcomed by the German Emperor into nobility with the title of "von" added to his name. These prestigious awards made his doctrine virtually unassailable in the scientific community.

Ampere's principle of transverse magnetic attraction and repulsion between electric currents had been made into an equation for the magnetic force between moving electric charges by Carl Fredrick Gauss (written in 1835, published posthumously in 1865). The critical part of the Gauss equation shows, and modern physics texts agree, that magnetic force is transverse to the force that imparts a relative velocity (i.e. perpendicular to a connecting line) between charges. Lacking a direct back-force, a transverse magnetic force can produce a greater force that the force that causes it.

The only physicist to recognise in print, the profound significance of the work of Gauss, was James Clerk Maxwell (1873), who stated "(If Gauss's formula is correct), energy might be generated indefinitely in a finite system by physical means". Prepossessed with Helmholtz's "law", Maxwell chose not to believe Gauss's transverse magnetic-force equation and accepted Wilhelm Weber's (1846) erroneous in-line formula instead. Maxwell even admitted knowing of Gauss's (1845) rebuke of Weber for his mistaken direction of magnetic force as "a complete overthrow of Ampere's fundamental formula and the adoption of essential a different one".

In 1893, the critical part of Ampere's formula for magnetic force, which Weber and Maxwell rejected, and which Helmholtz had replaced with his contrary metaphysical explanation, was proposed for the basis for the international measure of electric current, the Ampere (or amp), to be defined in terms of the transverse magnetic force which the current produces. But Helmholtz's doctrine had become so impervious to facts that anyone who challenged this "law" faced defamation and ridicule.

The first recognition of unlimited energy came from Sir Joseph Larmor who reported in 1897, "A single ion e, describing an elliptic orbit under an attraction to a fixed centre ... must rapidly lose its energy by radiation ... but in the cases of steady motion, it is just this amount that is needed to maintain the permanency of motion in the aether". Apparently to mollify critics of his heretical concept, Larmor offered a half-hearted recantation in 1900: "The energy of orbital groups ... would be through time, sensibly dissipated by radiation, so that such groups could not be permanent".

In 1911, Rutherford found that an atom resembles a small solar system with negative ions moving like planets around a small, positively charged nucleus. These endlessly orbiting electrons were a source of the perpetual radiation that had aptly been described by Larmor, and these orbiting electrons were also Planck's (1911) "harmonic oscillators" which he used to explain Zero-point Energy (ZPE). ZPE was shown by the fact that helium remains liquid under atmospheric pressure at absolute zero, so that helium must be pressurised

to become solid at that temperature. Planck believed that harmonic oscillators derived "dark energy" from the aether to sustain their oscillations, thereby admitting that an infinite source of energy exists. However, he assigned an occult origin to this infinite energy, rather than a conventional source that had not met with Helmholtz's approval.

Niels Bohr (1924) was bothered by the notion that radiation from an orbiting electron would quickly drain its energy so that the electron should spiral into the nucleus. Whittaker (1951) states, "Bohr and associates abandoned the principle ... that an atom which is emitting or absorbing radiation must be losing or gaining energy. In its place, they introduced the notion or virtual radiation, which was propagated in ... waves but which does not transmit energy or momentum". Subsequently, the entire scientific community dismissed Larmor radiation as a source of real energy because it failed to conform to Helmholtz's universally accepted doctrine.

Helmholtz's constraining idea that the vast amount of light and heat radiating from the many billions of stars in the universe can only come from previously stored energy, has led scientists to concur that fusion of preexisting hydrogen to helium, supplies nearly all the energy that causes light and heat to radiate from the sun and other starts. If so, then the entire universe will become completely dark after the present hydrogen supply in stars is consumed in about 20 billion years. William A. Fowler (1965) believed that essentially all the hydrogen in the universe "emerged from the first few minutes of the early high-temperature, high-density stage of the expanding Universe, the so-called 'big bang' ..." Moreover, the background energy of the universe was thought by some to be "relic" radiation from the "Big Bang".

To accept the Big Bang idea that all the stars in the universe originated at the same time, it was necessary to disregard the fact that most stars are much younger or much older than the supposed age of the one-time event, which indicates that their energy must have come from a recurring source. The Big Bang is entirely dependent on the idea that the whole universe is expanding, which stemmed from the interpretation that Hubble's red-shift with distance from the light source, represents a Doppler shift of receding stars and galaxies. This expanding-universe interpretation was shattered by William G. Tifft (1976, 1977), who found that observed red-shifts are not spread randomly and smoothly over a range of values, as would be expected from the Doppler shifts of a vast number of receding stars and galaxies. Instead, the observed red-shifts all fall on evenly spaced, quantised values.

Moreover, Shpenkov and Kreidik (2002) determined that the radiation temperature corresponding to the fundamental period of the orbital electron motion in the hydrogen atom of 2.7289⁰K matches the measured temperature of cosmic background radiation of 2.725⁰K plus or minus 0.002⁰K. This represents perpetual zero-level Larmor radiation from interstellar hydrogen atoms dispersed in the universe. So, Helmholtz's idea that "the energy in the universe is a fixed amount immutable in quantity from eternity to eternity" does not stand up to known facts.

The large aggregate quantity of heat-photons which is generated continually by Larmor radiation can account for the illumination of stars and for the enormous heat and pressure in active galactic centres. Based on the fact that photons exhibit momentum, photons must posses mass, because, as Newton explained, momentum is mass times velocity, which in this case is "c". Consequently, the creation of photons by induction or by Larmor radiation, also creates new mass. The conditions that Fowler was seeking for hydrogen nucleosynthesis, are apparently being supplied indefinitely in active galaxies and possibly in the sun and other stars above a certain size. This invention utilises a similar unlimited energy source.

Another principle that is important to this specification, is that the transfer of energy by electrical induction was found by the Applicant to work in the same manner as the transfer of energy by broadcast and reception of oscillating radio signals. A transverse force is communicated in both cases, the force declines similarly with distance, and the effects of shielding and reflection are identical. Since radio signals are communicated by photons, Applicant considers that inductive force is also communicated by photons. The radiation of newly formed inductive photons results when an accelerated charge experiences a change in direction of acceleration. Inductive radiation occurs when the acceleration of electric charges is reversed, as in Rontgen's bremsstrahlung, in Hertz's linear oscillator (plus all other radio-broadcasting antennas), and in coils which carry an alternating current.

In a similar case, when electric charges move in a curving motion due to a continually changing centripetal acceleration, inductive photons are radiated steadily. This includes the radiation from electrons orbiting atomic nuclei (Larmor radiation) and from conduction electrons flowing in a wire coil, whether the current is steady or not. Circularly produced inductive photons induce a circular motion (diamagnetism) in mobile electrons located near the axis of the electron's circular movement.

In both the reverse-acceleration and centripetal-acceleration cases, inductive photons convey a force to mobile electrons that is transverse to the photon's propagation path. As Lapp and Andrews (1954) reported,

"Low-energy photons produce photoelectrons at right angles to their path ...". This same right-angle force without a direct back-force, applies as well, to all conduction electrons which are accelerated by low-energy photons. Hence, inductive energy qualifies for exemption from the energy-conservation law by Helmholtz's same ad infinitum principle which exempts magnetic energy.

The transverse force that inductively produced photons delivered to mobile electrons, is opposite in direction to the simultaneous movement of the primary charge which produces the radiation. This is shown by Faraday's induced current opposite to the inducing current and by the diamagnetically-induced circular motion which, in a rotational sense, is opposite to the circular electron motion in the coil producing it. An oscillating flow of electrons within a loop of a wire coil, induces a force on the conduction electrons which is in the opposite direction in adjacent loops of the same wire. This results in self-induction.

Important to this specification is the realisation that the energy transmitted by photons is kinetic rather than electromagnetic. Inductively radiated photons of low energy, light rays and X-rays cannot be deflected by and electric or magnetic field due to the photons' neutral charge. Neither do neutral photons carry an electric or magnetic field with them. Photon radiation is produced by a change in the acceleration of an electric charge, so only in special cases does it have an electrokinetic origin which involves a magnetic force. To honour these facts, Applicant uses the term "electrokinetic spectrum" in place of "electromagnetic spectrum".

Another principle which is important to this specification is the realisation that, although the charge on the electron has a constant value under all conditions, the mass of an electron is not a fixed, unchanging amount. All free electrons, as in cathode rays, have exactly the same amount of mass at sub-relativistic velocities. This is called "normal" mass and is denoted by m_e. Free electrons have a unique charge to mass ratio that makes the magnetic force resulting from a sub-relativistic velocity imparted to such an electron, exactly equal to the energy input with "normal" electrons.

Also, when a normal electron is given a sub-relativistic acceleration, the inductive force it produces is equal to the force it receives. The mass of highly conductive electrons of metals is apparently very close to normal, but any very slight inductive-energy gains would be masked by inefficiencies. The ubiquity of free electrons and the conduction electrons of metals has led to the view that electron mass is a never-varying figure that would allow the energy conservation law to apply to magnetic energy and inductive energy.

Accurate determinations of electron mass in solid materials have been made possible by cyclotron resonance, which is also called diamagnetic resonance. The diamagnetic force produced by the steady flow of electrons in a wire coil, induces the mobile electrons of a semiconductor to move in a circular orbit of indefinite radius but at a definite angular frequency. This frequency is only related to the inductive force and the mass of the electron. At the same time, a repulsive magnetic force is developed by the relative velocity between the electron flow in the coil and the conduction electrons, causing the mobile electrons of the semiconductor to move in a helical path away from the coil rather than in planar circles. Only two measurements are needed to determine the mass of such an electron: the cyclotron frequency which is determined by the current and dimensions of the coil. Since the co-produced magnetic field is related to the same parameters, its measurement serves as a surrogate for inductive force.

Because the measured mass of conduction electrons in semiconductors is less than normal, a complicated explanation has been adopted to defend the constancy of electron mass in order to support Helmholtz's energy doctrine. An extra force is supposedly received from the vibrational lattice-wave energy of the crystal (in what would have to be an act of self-refrigeration) to make normal-mass electrons move faster than expected around a circular path, thereby giving the appearance that the electron has less mass than normal. In this explanation, the electron is considered to be a smeared-out wave rather than a particle, which is contradicted by the billiard-ball-like recoil of an electron when it is bumped by a quantum of radiation, as described by Arthur Crompton and Samuel Allison (1935).

The fallacy that borrowed energy can provide a boost in velocity to an electron, is more apparent in the case of linear motion. The effective-mass theory considers that the greater linear velocity is caused by a boost given to normal-mass electrons by a "longitudinal wave" imparted by an externally applied force in the same direction as the electron motion. Since this longitudinal wave is also considered to have a source in crystal-lattice vibrations, the effective-mass theory relies on a reversal of entropy in violation of the second Law of Thermodynamics.

No reasonable contribution of direct directional energy can be invoked from any source to impart abnormally great velocity to the conduction electrons in semiconductors. So, the operation of apparatus embodiments described herein, relies on electrons having particle properties and on electrons having less-then-normal inertial mass without invoking any special forces. This is supported by Brennan's (1999) statement that "the complicated problem of an electron moving within a crystal under the interaction of a periodic but

complicated potential, can be reduced to that of a simple free particle, but with a modified mass". The term "effective" is herein considered redundant in referring to truly inertial mass, but "effective mass" still has relevance in referring to the net movement of orbital vacancies or "holes" in the opposite direction of low-mass electrons.

By F = ma, a low-mass electron receives greater acceleration and greater velocity from a given force than an electron of normal mass. The velocity and kinetic energy imparted to an electrically charged body by a force, are determined by the electric charge without regard to the body's mass. Having a smaller amount of mass, allows a body to attain a greater velocity with any given force. Hence, the magnetic force produced by the charge at this higher velocity will be greater than it would normally be for that same amount of force. This allows low-mass electrons to produce a magnetic force that is greater than the applied force.

Also, the amount of inductive radiation energy from accelerated electrons is related to an electron's charge without regard to its mass. The energy of inductive radiation increases with the square of the electron's acceleration according to Larmor's (1900) equation, while the acceleration is inversely proportional to the lesser electron mass relative to normal electron mass. Therefore, the greater-than-normal acceleration of low-mass electrons, allows the re-radiation of magnified inductive-photon energy at a magnification factor which is proportional to the inverse square of the electron's mass, e.g., the inductive-energy magnification factor of cadmium selenide photoelectrons with 0.13 of the normal electron mass is (0.13)² which is 59 times.

Electrons appear to acquire or shed mass from photons in order to fit the constraints of particular orbits around nuclei, because each orbit dictates a very specific electron mass. In metals, where the conduction electrons seem to move as would a gas, one might think that they would assume the normal mass of free electrons. But the largest mean free path of electrons in the most conductive metals is reportedly about 100 atomic spacings between collisions (Pops, 1997), so the conduction electrons apparently fall back into orbit from time to time and thereby regain their metal-specific mass values.

As conduction electrons pass from one metal type to another, they either lose or gain heat-photons to adjust their mass to different orbital constraints. In a circuit comprising two different metallic conductors placed in series contact with each other, the flow of conduction electrons in one direction will cause the emission of heat-photons at the junction, while an electron flow in the reverse direction causes cooling as the result of ambient heat-photons being absorbed by the conduction electrons at the junction (Peltier cooling effect). When a metal is joined with a semiconductor whose conductive electrons have much lower mass than in metals, much greater heating or cooling occurs at their junction.

John Bardeen (1941) reported that the (effective) mass of superconducting electrons in low-temperature superconductors is only 10^{-4} as great as the mass of normal electrons. This is demonstrated when superconducting electrons are accelerated to a much higher circular velocity than normal in diamagnetically induced eddy currents, which results in enormous magnetic forces which are capable of levitating heavy magnetic objects. Electrons with 10^{-4} times normal mass are apparently devoid, (or nearly devoid) of included photon mass, so normal electrons are deduced to posses about 10^{4} times more included photon mass than the bare electron's own mass.

The means by which photon mass may be incorporated within, or ejected from electrons, can be deduced from known information. Based on the Thompson scattering cross-section, the classical radius of a normal electron is 2×10^{-15} cm. If the electron has uniform charge throughout a sphere of that radius, the peripheral velocity would greatly exceed the velocity of light in order to provide the observed magnetic moment. Dehmelt (1989) determined that the radius of the spinning charge which creates an electron's magnetism, is approximately 10^{-20} cm. This apparent incongruity can be explained if the electron is considered to be a hollow shell (which is commensurate with the bare electron's tiny mass in comparison to the very large radius) and if the negative charge of the shell is not the source of the magnetic moment.

It has long been known that a photon can be split into an negative ion (electron) and a positive ion (positron), each having the same amount of charge but of opposite sign. Electrons and positrons can recombine into electrically neutral photons, so it is apparent that photons are composed of a positive and a negative ion. Two ions spinning around each other could produce the photon's wave nature. The only size of photon ion that can exist as a separate entity has a charge of exactly plus one or minus one, whereas the ions can have a very much larger or very much smaller charge and mass when combined in photons, as long as the two ions are equal in charge and mass. Combined in a photon, the two ions are apparently attracted together so strongly that their individual volumes are very much smaller than as separate entities.

When a dipole photon enters an electron shell, its negative-ion portion is expected to be forced towards the shell's centre by Coulombic repulsion, while the photon's positive ion would be attracted by the negative charge of the shell equally in all directions. The negative photon ions would likely merge into a single body

at the electron's centre, while the positive-ion portion would orbit around the centralised negative ion to retain the photon's angular momentum. The high peripheral velocity of this orbiting photon mass would enable portions of photon material to spin off and exit the electron shell at the same velocity at which they entered the electron, i.e., the speed of light. The orbiting of the positive photon charge at Dehmelt's small radius, most likely accounts for the magnetic moment that is observed in electrons of normal mass.

Liberated low-mass conduction electrons within intrinsic semiconductors (which are also photoconductors by their nature) and within doped semiconductors, are mostly protected against acquiring mass from ambientheat photons by the heat-insulative properties of the semiconductors. In contrast, low-mass electrons injected into heat-conducting metals, rapidly acquire mass from ambient-heat photons by the existence of cryogenic conditions, but they are vulnerable to internal heat-photons created by excessive induction.

Conduction electrons of metals, typically move as a group at drift velocities of less than one millimetre per second, although the velocity of the electrical effects approaches the velocity of light. (Photons are probably involved in the movement of electrical energy in metallic conductors.) In contrast, conductive low-mass electrons can move individually at great velocities in superconductors and semiconductors. Brennan (1999, p. 631) reports the drift velocity of a particular electron moving in a semiconductor, to be one micrometer in about 10 picoseconds, which is equivalent to 100 kilometers per second.

The concentration of the conduction electrons in metals is the same as the number of atoms, whereas in semiconductors, the mobile low-mass electrons which are free to move, can vary greatly with the amount of certain photon radiation received. Since the magnitude of an electric current is a summation of the number of electrons involved, times their respective drift velocities, the current developed by a small ensemble of photoconducting electrons moving at high speed, can exceed the current of a much greater number of conduction electrons moving at a very low speed in a metal.

A general feature of intrinsic semiconductors is that they become photoconductive in proportion to the amount of bombardment by some particular electron-liberating frequency (or band of frequencies) of photon energy, up to some limit. The amount of bombardment by the particular wavelength (or, equivalently, the frequency), increases along with all other photon wavelengths as the ambient temperature rises, that is, as the area under Planck's black-body radiation curve increases. Consequently, the conductivity of semiconductors continues to increase with temperature, while the conductivity drops to almost zero at low temperature unless superconductivity occurs.

A single high-energy alpha particle can liberate a great number of low-mass electrons in a thin-film semiconductor, as Leimer's (1915) energy-magnifying experiment appears to show. Leimer's alpha radiation was situated near the distant end of a suspended antenna wire of unreported length, when he experienced the maximum magnetic energy increase in the coil of the ammeter in the receiver. The low-mass electrons had to have travelled the entire length of the suspended antenna and the connecting line to his receiving apparatus without encountering any trapping holes. Assuming these electrons traversed a distance of 1 to 10 metres in less than one half-cycle of the radio frequency, (that is, less than 4 microseconds at 128 kHz) at which time the direction of the low-mass electron would have been reversed, this would be equivalent to velocities of 25 to 250 km/sec.

A great number of superconducting electrons can be set in motion by inductive photon radiation. In contrast, inductive photon radiation can pass mostly through photoconductors that have low concentrations of mobile, low-mass electrons. Applicant's interpretation of Leimer's experiment is that the liberated low-mass electrons of the semiconductor coating of the antenna wire, were not directly accelerated by the inductive photons of the radio signal, but rather were accelerated to high velocities by an oscillating electric field created in the metallic wire by the radio photons.

A review of an experiment performed by File and Mills (1963), shows that the very low mass of superconducting electrons is responsible for causing supercurrents to differ from normal electric currents. A superconducting solenoidal coil (comprising a Nb-25% Zr alloy wire below 4.3⁰ K.) with the terminals spotwelded together to make a continuous conductor, was employed. Extremely slow declines of induced supercurrents were observed, which can be attributed to an enormous increase in the coil's self-induction. Because a supercurrent approaches its maximum charge asymptotically when discharging, a convenient measure of the coil's charging or discharging rate is the "time-constant". The time-constant has the same value for both charging and discharging, and it is defined as (a) the time needed for charging the coil to 63% of the maximum amount of current inducible in the coil by a given diamagnetic force, or (b) the time needed to discharge 63% of the coil's induced current.

In normal conductors, the inductive time-constant is calculated by the inductance of the coil, divided by the resistance of the coil. By use of an empirical equation, the inductance of the coil in its non-superconducting state is calculated to be 0,34 Henry, based on a double-layered solenoid of 384 turns that measured 4 inches (10 cm) diameter and 10 inches (25 cm) long. The resistance of the 0.020 inch (0.51 mm) diameter

wire at a temperature of 5^{0} K. (just above T_c) is estimated by using data for Zr alone, to be 4 x 10^{2} ohms. (Resistivity data were not available for Nb or the subject alloy). Under non-superconducting conditions, the time-constant for charging and discharging this coil is thereby calculated to be approximately 8 x 10^{-5} sec.

The time it took to charge up a supercurrent in the coil in the experiment was not reported. But, based on the reported 50 re-energisings and magnetic determinations performed in 200 hours, the measured charging time in the superconducting state is computed to be no more than 4 hours on average.

Using Bardeen's (1941) formula of m is approximately equal to m_e times 10^{-4} for the order of magnitude of the low T_c superconducting electron's mass, and using Larmor's equation (1900) which relates inductive radiation power to the square of the acceleration of the charge, the inductance of the coil is expected to increase by $(10^4)^2 = 10^8$ times in the superconducting state. Thus, the calculated increase in the time-constant of charging up the supercurrent is $8 \times 10^{-5} \times 10^8$ which equals 8×10^3 seconds, or 2.2 hours, which is the same order of magnitude as the maximum actual charging time. The self-induction increased by that amount because the low-mass electrons are accelerated 10^4 times faster.

In the case of discharging, the time constant of the supercurrent was projected by File and Mills from measured declines observed over periods of 21 and 37 days. The projections of the two 63% declines agreed closely at 4 x 10^{12} seconds (= 1.3×10^5 years). Therefore, the time-constant of supercurrent discharge, based on projecting actual measurements, had increased by 5 x 10^{16} times over the time-constant for electrons of normal mass.

The driving force during charging, had been the applied inductive force, whereas the driving force during discharging was the supercurrent that had been magnified 10^8 times. Therefore, during the discharging of the supercurrent, the time-constant is increased again by 10^8 times, so the calculated total increase in the time-constant of discharge is $10^8 \times 10^8 = 10^{16}$ times greater than the normal time-constant. This calculated value of the non-superconducting time-constant, based solely on the increase of inductive radiation due to extremely low electron mass, compares favourably in magnitude with the actually observed value of 5 x 10^{16} times the normal time-constant.

The superconducting coil required no more than four hours to charge up the supercurrent, yet during subsequent discharge, the superconducting coil was projected to radiate inductive photon energy from the centripetal acceleration of the superconducting electrons for 130,000 years before declining by 63%. If this experiment could take place where no energy would needed to sustain critical cryogenic conditions, as in outer space, the lengthy discharge of this energised coil would clearly demonstrate the creation of energy in the form of newly-created photons inductively radiating from the superconducting low-mass electrons that circulate around the coil's loops. Applicant interprets this as showing that low-mass electrons are capable of inductive-energy-magnification based solely on their mass relative to that of normal electrons.

In the embodiments described below, the magnified inductive energy of low-mass electrons is utilised in coils for electric-energy generation by employing a flow of inductively accelerated photons that alternates in direction. This, in turn, drives low-mass electrons in an oscillating manner, so this forced reversal involves only a single stage of inductive-energy magnification, rather than the two stages (charging and naturally discharging) in the foregoing experiment.

Mode of Operation

Inductive photons radiating from an oscillating electric current in a sending conductor (e.g. from a radio-wave broadcasting antenna) convey a force, on conduction electrons in a receiving conductor, that is transverse to the incidence direction of the incident inductive photons on the receiving conductor. As a result, no backforce is transferred directly back to the sending conductor. Applicant has discovered that the action of this transverse force on low-mass electrons in a receiving conductor is analogous to the action of Gauss's transverse magnetic force on free electrons in a conductor, which is not subject to the kinetics law of conservation of energy. If the receiving conductor has low-mass electrons than that it would impart to normal free electrons. The resulting greater drift velocities of low-mass electrons than normal free electrons in the receiving conductor, would yield an increased magnitude of inductive force produced by the low-mass electrons in the receiving conductor and hence produce a magnification of the irradiation energy of inductive photons.

The direction of the transverse force imparted by the radiated inductive photons on conduction electrons in the receiving conductor is opposite to the direction of the corresponding electron flow in the sending conductor. This relationship is similar to the inductive force on electrons in the secondary coil of a transformer, which also is opposite to the direction of flow of electrons in the primary coil.

Various embodiments of Applicant's electrical generator employ inductive photons radiated from electrical oscillations in a "sending coil". Inductive photons are radiated from the sending coil toward and inductive-photon receiving coil, termed an "energy-magnifying coil", which comprises a photoconductive or superconductive material, or other suitable material as described below. The energy-magnifying coil is placed in a condition favourable for the production of low-mass electrons that participate in electrical conductive material, the coil is provided with a photoconduction exciter. Alternatively, if the energy-magnifying coil is made of photoconductive material, the coil is provided with a photoconduction exciter. Alternatively, if the energy-magnifying coil is made of a superconductive material, the coil is placed in an environment at a temperature (T) no greater than the critical temperature (T_c); i.e., T < T_c. In the former example, the photoconduction exciter can be a source of illumination which provides an appropriate wavelength of excitive electrokinetic radiation. If the energy-magnifying coil is comprised of a doped semiconductor, the condition that provides mobile low-mass electrons already exists.

In the energy-magnifying coil, the greater-than-normal acceleration of the low-mass electrons produces greater-than-normal inductive forces in the form of greater-than-normal radiation of inductive photons from the coil. The resulting increased inductive-photon energy from the photoconductor or superconductor is converted into useful electrical energy in an output coil inductively coupled to the energy-magnifying coil. The output coil can be made of insulated metallic wire. An exemplary output coil is situated coaxially with, and nested within, the energy-magnification coil. A coil of this type is termed herein, an "internal output coil".

The ability of the subject apparatus to produce more energy output than energy input, is based on the output coil receiving more of the magnified energy from the energy-magnifying coil than is returned as a back-force from the output coil to the energy-magnifying coil. This principle is termed herein "energy leverage".

The oscillations in the energy-magnifying coil are initiated by an external energy-input source that provides an initiating impulse of electron flow in the sending coil. For example, the external energy-input source can be an adjacent independent electromagnet or an adjacent permanent magnet moved rapidly relative to the sending coil. The initiating impulse starts an oscillation in the sending coil that stimulates radiation of inductive photons from the sending coil to the energy-magnifying coil. Energy from the external energy-input source is magnified by the apparatus so long as the energy-magnifying coil does not act as an independent oscillator at a different frequency. Independent oscillation is desirably avoided by connecting the ends or terminals of the energy-magnifying coil to each other in such a way that it results in one continuous coil, or a continuous multiple-coil system or systems, connected together in such a way that continuity exists for the conduction of low-mass electrons throughout the entire coil system. The energy-magnifying coil inductively creates more energy in the output coil than the energy of the initial impulse. The resulting magnified output of electrical energy produced by the apparatus is available for useful purposes in a work loop.

After initiation, the apparatus is made self-sustaining using a feed-back loop arranged in parallel with the work loop that includes the sending coil, and with a capacitor located in the feed-back loop to make it an L-C circuit, i.e., after start-up of the apparatus using the external energy-input source, the apparatus becomes self-resonating, which allows the external energy-input source to be decoupled from the apparatus without causing the apparatus to cease production of electrical energy.

During normal self-sustained operation, a portion of the output electrical energy is returned to the sending coil by the feed-back loop, thereby overcoming the need to use the external energy-input source for sustaining the oscillations in the sending coil. In other words, after startup, the external energy which was used by the sending coil to excite the photoconductive material or the superconducting material in the energy-magnifying coil is replaced by a portion of the output energy produced by the apparatus itself. The remainder of the output electrical energy is available in the work loop for useful purposes.

Initiating the generation of electrical energy by the apparatus, takes advantage of the fact that the inductive back-force sent from the output coil to the energy-magnifying coil (and hence ultimately, back to the sending coil), arrives at the sending coil one cycle behind the corresponding pulse that initiated the flow of electrons. This one-cycle lag of the back-force, as well as a corresponding one-cycle lag in the feed-back, enables small starting pulses produced in the sending coil to produce progressively greater electrical outputs each successive cycle. Consequently, assuming that the electrical load is not excessive during start-up, only a relatively few initiating cycles from the external energy-input source typically are needed for achieving production by the apparatus of an amount of output power sufficient to drive the load as well as providing sufficient energy feed-back to the sending coil in a sustained manner.

A half-cycle of the one-cycle lag occurs between an initial acceleration of electrons in the sending coil and a corresponding initial oscillation in the energy-magnifying coil. This half-cycle lag occurs because induction photons are not radiated from the initial acceleration of electrons in the sending coil, but rather are radiated when the electrons are reverse-accelerated. (Kramers, 1923, and Compton and Allison, 1935, p.106). As the newly formed photons are being radiated by the respective deceleration of electrons in the sending coil, even more new photons are simultaneously being formed by the new direction (i.e. reverse direction) of

acceleration under oscillating conditions. Thus, the radiation of photons from electrons alternatingly accelerated in the opposite direction from the conveyed force, continues each half-cycle after the initial half-cycle.

Applicant also discovered that a half-cycle lag also occurs between the initial flow of electrons in the primary coil of a certain type of transformer, which is simply comprised of coils nested coaxially rather than being inductively coupled by an iron core, and the resulting electron flow induced in the secondary coil. When applied to this apparatus, these finding indicate that a second half-cycle lag occurs between the acceleration of low-mass electrons in the energy-magnifying coil and the corresponding electron flow induced in the output coil. The feed-back from the output coil boosts the electron flow in the sending coil one whole cycle after the initial pulse.

As discussed above, the energy-magnifying coil comprises either a photoconductor, a doped semiconductor or a superconductor as a source of, and as a conductor of, low-mass electrons. The general configuration of the coil is similar in either case. The coil including a photoconductor or doped semiconductor, has an operational advantage at normal temperatures, and the coil including a superconductor has an operational advantage at sub-critical temperatures (T < T_c), such as in outer space.

Representative Embodiments



Reference is now made to **Fig.1A** to **Fig.1C** and **Fig.2A** and **Fig.2B** which depict a sending coil **20** connected to a source of alternating current **21**. The sending coil is shown having a desirable cylindrical profile, desirably with a circular cross-section as the most efficient configuration. In **Fig.1A** and **Fig.1B**, electrical oscillations from the source **21** are conducted to the sending coil **20** where they cause inductive photons **22** to radiate from the sending coil. The radiated photons **22** convey transverse forces in the same manner that a radio-broadcasting antenna transmits oscillating energy. The sending coil **20** can be a single layer or multiple layers of insulated metal wire (e.g. insulated copper wire). One layer is sufficient, but an additional layer or layers may increase operational efficiency. If necessary, or desired, the turns of wire can be formed on a cylindrical substrate made of a suitable dielectric.

24

25b

26

The inductive photons 22 radiating from the sending coil 20, propagate to an energy-magnifying coil 24 that desirably has a cylindrical profile extending parallel to the sending coil. In the embodiment shown in Fig.1A and Fig.1B, the energy-magnifying coil 24 does not terminate at the ends, but rather, it is constructed with a connector 30 to form a continuous conductor. The energy-magnifying coil 24 desirably is a helical coil made

of a material comprising a photoconductive or superconductive material, or other suitable material. If necessary or desired, the energy-magnifying coil can be formed on a substrate which, if used, desirably is transmissive to the inductive-photon radiation produced by the coil.

In an energy-magnifying coil **24** made of a superconducting material, a large population of conductive lowmass electrons is produced in the coil by lowering the temperature of the coil to a point below the critical temperature for that material. By way of an example, sub-critical temperatures are readily available in outer space or are produced under cryogenic conditions.

In an energy-magnifying coil 24 made of a photoconductor material, a large population of conductive lowmass electrons is produced in the coil by illuminating the coil with photons of an appropriate wavelength, such as photons produced by a photoconduction exciter 26. The photoconductor exciter 26 desirably is situated and configured so as to illuminate substantially at least the same side of the energy-magnifying coil 24 that receives inductive photons 22 radiating directly from the sending coil 20. Alternatively, the photoconduction exciter 26 can be situated and configured so as to illuminate all sides of the energymagnifying coil 24. In the depicted embodiment, the photoconduction exciter 26 can be at least one incandescent lamp (as shown) energised by conventional circuitry (not shown). Alternatively, the photoconduction exciter 26 can be at least one gas-discharge lamp or one or more Light Emitting Diodes. The wavelength produced by the photoconduction exciter 26 can be, for example, in the infrared (IR), visible, ultraviolet (UV), or X-ray range as required by the particular photoconductor material in the energymagnifying coil 24. Another possible form of the photoconduction exciter 26, is a source of photons in the gigahertz or the terahertz portion of the electrokinetic spectrum. Other photoconduction exciters are configured, as required, to produce a suitable wavelength from the radio-wave portion of the electrokinetic spectrum. The illumination can be either direct from the photoconduction exciter 26 to the energymagnifying coil 24 or conveyed from a remotely located photoconduction exciter to the energy-magnifying coil via optical fibres, light pipes, or the like.

Fig.1B and **Fig.1C** are respective orthogonal end views of the sending coil **20** and energy-magnifying coil **24** shown in **Fig.1A**. The radiation of inductive photons **22** from the sending coil **20**, is indicated schematically in **Fig.1A**, **Fig.1B** and **Fig.1C** by small, jagged arrows. The forces delivered by the photons **22** to the conductive low-mass electrons in the energy-magnifying coil **24**, alternate in directions which are opposite to the respective directions of simultaneous electron flow in the sending coil **20**. Whenever the particular oscillation phase of electron flow in the sending coil **20** is in the direction of the curved arrow **25a** adjacent to the sending coil **20** in **Fig.1B**, the resulting transverse photon force causes a flow of low-mass electrons in the energy-magnifying coil **24**, adjacent to the energy-magnifying coil **24**, depicted by the curved arrow **27a** adjacent to the energy-magnifying coil **24**.

The shaded sector **29**, shown in **Fig.1B**, denotes the proportion of inductive-photon radiation **22** from the sending coil **20**, actually received by the single energy-magnifying coil **24** shown, compared to the entire 360-degree radiation of inductive photons **22** from the sending coil **20**. Aside from a small amount of inductive-photon radiation lost from the ends of the sending coil **20**, the relative amount of the total energy of inductive-photon radiation received by the energy-magnifying coil **24** is determined by the angle subtended by the energy-magnifying coil **24**, relative to the entire 360 degrees of inductive-photon radiation from the sending coil **20**.

In **Fig.1C**, the low-mass conduction electrons of the energy-magnifying coil **24** are accelerated to a higher drift velocity than normal free electrons in the energy-magnifying coil **24** would be. As noted above, the sending coil **20** is energised by alternating electron flow, which causes a periodic reversal of direction of electron flow in the sending coil **20** (compare the direction of the arrow **25b** in **Fig.1C** with the direction of the arrow **25a** in **Fig.1B**). Each reversal of direction of electron flow in the sending coil **20**, causes a corresponding reversal in the direction of acceleration of the low-mass electrons in the energy-magnifying coil **24** (compare the direction of acceleration causes a corresponding radiation of an **Fig.1B**). Each such reversal in direction of acceleration causes a corresponding radiation of inductive photons (jagged arrows **18a**, **18b**) radially outwards and radially inwards, respectively, from the energy-magnifying coil **24**. Note that the arrows **18a** and **18b** are larger than the arrows denoting the inductive photons (arrows **22**) from the sending coil **20**. This symbolically denotes energy magnification. Note also that, of the magnified inductive-photon energy radiating from the energy-magnifying coil **24**, substantially half is directed inwards (arrows **18b**), and substantially the other half is radiated outwards (arrows **18a**).



Turning now to **Fig.2A**, the sending coil **20**, and the energy-magnifying coil **24**, are shown. The energymagnifying coil **24** in **Fig.2A** includes an internal output coil **28a**, that desirably is situated co-axially inside and is of the same length as the energy-magnifying coil **24**. A work loop **48** can be connected to the ends of the internal output coil **28a**, thereby forming an electrical circuit in which a load **49** is indicated symbolically as a resistor. The internal output coil **28a** and the conductors of the work loop **48**, desirably are made of insulated metallic (e.g. copper) wire.



Fig.2B depicts a transverse section of the coils shown in **Fig.2A**. In **Fig.2B**, the magnified inductive-photon energy (shaded area **19**) produced by the energy-magnifying coil **24** and directed radially inwards towards the internal output coil **28a**, induces a corresponding oscillating electron flow in the internal output coil **28a**. Thus, the work loop **48** connected across the internal output coil **28a**, is provided with greater energy than was received by the energy-magnifying coil **24** from the sending coil **20**. The direction of the electron flow (arrow **17**) in the internal output coil **28a**, is opposite to the direction of flow (arrow **27b**) in the energy-magnifying coil **24**, which in turn is opposite to the direction of electron flow **25b** in the sending coil **20**.

In **Fig.2B**, the annular-shaped shaded area 19 between the energy-magnifying coil **24** and the internal output coil **28a**, indicates that substantially all of the internally-directed magnified inductive-photon energy (i.e. approximately half of the total radiation energy) from the energy-magnifying coil **24**, is directed to, and captured by, the internal output coil **28a**. In contrast, the shaded sector **16** extending from the energy-magnifying coil **24** to the sending coil **20**, indicates that a relatively small proportion of the outwardly directed magnified radiation **18a** from the energy-magnifying coil **24** is directed to the sending coil **20** where the radiation provides a corresponding back-force. Aside from the small amount of inductive-photon radiation lost from the energy-magnifying coil **24**, the relative amount of the magnified inductive-photon radiation (sector **16**) providing the back-force on the sending coil **20**, is a function of the angle subtended by the sector **16**, compared to the 360-degree radiation from the energy-magnifying coil **24**.

The ratio of magnified energy **18b** from the energy-magnifying coil **24** and received by the internal output coil **28a**, to the magnified energy **18a** received as a back-force by the sending coil **20**, denotes the energy "leverage" achieved by the subject apparatus. If this ratio is greater than unity, then the energy output from the internal output coil **28a** exceeds the energy input to the energy-magnifying coil **24**. This energy leverage is key to the self-sustained operation of the apparatus, especially whenever the apparatus is being used to drive a load. In other words, , with a sufficiently large energy-magnification factor achieved by the energy-magnifying coil **24**, the electrical energy available in the work loop **48**, exceeds the input energy that produces the oscillations in the sending coil **20**. The electric power input to the sending coil **20** thereby

produces magnified electric power in the internal output coil **28a** that can perform useful work in the work loop **48** while self-powering the continued operation of the apparatus.



Reference is now made to **Fig.3**, which schematically depicts aspects of the apparatus **15**, responsible for self-generation of electric power by employing a feed-back loop **46**. The conductors of the feed-back loop **46** can be made of insulated metallic wire. (In **Fig.3**, the dotted lines **47a** and dotted arrow **47b**, indicate that the internal output coil **28a** is actually positioned co-axially inside the energy-magnifying coil **24**, as described above, but is depicted in the figure as being outside the energy-magnifying coil for ease of illustration). The feed-back loop **46**, conducts a portion of the electric power from the internal output coil **28a**, back to the sending coil **20**. The remaining portion of the electric power from the internal output coil **28a** is directed to the work loop **48** where the power is utilised for useful work **51**. The relative proportions of output power delivered to the feed-back loop **46** and to the work loop **48**, can be varied by adjusting a variable resistor **50**.

As noted above, an initial source of electrical energy is used for "starting" the apparatus **15** by initiating an oscillation in the sending coil **20**. After starting, under usual operating conditions, the apparatus **15** is self-resonant and no longer requires the input of energy from the initial source. The particular inductance and distributed capacitance of the sending coil **20**, plus all other capacitances and inductances in the apparatus, provide a certain corresponding frequency of self-resonating oscillation. In the feed-back loop **46** is a capacitor **77** that makes the apparatus an L-C circuit which oscillates at its own frequency. the frequency can be changed by altering the capacitance or inductance of the apparatus, or both. the capacitor **77** can be a variable capacitor by which the frequency can be adjusted.

As shown in **Fig.3**, the initial source of oscillating electrical energy can be an impulse from an external electromagnet **52** powered by its own energy source (e.g. a battery **53** as shown, or other DC or AC source). For example, the electromagnet **52** can be placed near the sending coil **20** or other portion of the feed-back loop **46**, and energised by a momentary discharge delivered from the battery **53** via a switch **57**. The resulting pulse generated in the electromagnet **52**, initiates a corresponding electrical pulse in the sending coil **20** that initiates self-sustaining oscillations in the apparatus **15**. In another embodiment, the electromagnet **52** can be energised briefly by an AC source (not shown). In yet another embodiment, the initial source can be a permanent magnet which is moved rapidly (either mechanically or manually) near the sending coil **20** or other portion of the feed-back circuitry. In any event, the pulse provided by the initial source initiates electrical oscillations in the sending coil **20** that produce corresponding oscillating inductive-photon radiation **22** from the sending coil **20** causes, in turn, re-radiation of magnified inductive-photon energy **18b** from low-mass electrons in the energy-magnifying coil **24**, as shown schematically in **Fig.3** by thick jagged arrows. **Fig.3** depicts a photoconductive energy-magnifying coil **24** which is

illuminated by an incandescent photoconduction exciter **26** energised by its own power source **55** (e.g., an externally connected battery as shown).

A sufficiently high energy-magnification factor of the apparatus **15** allows the magnified energy from the energy-magnifying coil **24** to induce greater energy in the internal output coil **28a** than the energy of the corresponding initial pulse. A portion of the magnified electrical energy is returned to the sending coil **20** via the feed-back loop **46** to sustain the oscillations.

The remaining surplus energy from the internal output coil **28a** is available for application to useful work via the work loop **48**. In one embodiment, some of this useful work can be used for illuminating the photoconduction exciter **26** (circuitry not shown) in an apparatus configuration in which the energy-magnifying coil **24** comprises a photoconductor. In another embodiment, some of this useful work can be used for maintaining cryogenic ($T < T_c$) conditions for an apparatus configuration in which the energy-magnifying coil **24** comprises a semiconductor.

After starting oscillations in the apparatus **15**, electron flow builds up rapidly, so long as the load **49** does not draw off too much of the output energy during start-up. Upon reaching operating equilibrium, the output of electrical power from the apparatus **15** is a rapidly alternating current (AC). The AC output can be rectified by conventional means to produce direct current (DC), and the output can be regulated as required, using conventional means. Many variations of conventional circuitry are possible, such as, but not limited to, automatic voltage controllers, current controllers, solenoidal switches, transformers, and rectifiers,

Regarding the energy-magnifying coil **24**, an exemplary embodiment can be made from a low - T_c superconductor such as commercially available, flexible, niobium-zirconium wire which can be readily formed into a coil.. Other embodiments, as noted above, of the energy-magnifying coil **24** can be made using a photoconductive material or a high - T_c superconductor. Most high - T_c superconductors (and some photoconductors) have ceramic-like properties and thus require the application of special methods for forming the material into a cylindrical coil having electrical continuity throughout. Some commercially available high - T_c superconductors are available in ribbon or tape form. The energy-magnifying coil **24** can be free-standing or supported on a rigid substrate.

By way of example, an energy-magnifying coil **24** can be made from a ribbon of flexible photoconductive material such as the material discussed in patent US 6,310,281, incorporated herein for reference. Briefly, a layer of stress-compliant metal is placed on a plastic ribbon. Then the photoconductive material is deposited on both sides of the metal-covered ribbon and the edges of the ribbon so that the ribbon is coated all the way around. Such a configuration allows low-mass electrons in the photoconductive material, to receive energy from inductive-photons emitted from the sending coil **20** on one side of the ribbon while re-radiating magnified energy from both sides of the ribbon.

In another example, a flexible photoconductor ribbon is made from flexible organic polymer having photoconductive properties. (High electrical conductivity observed in photoconductive polymers is attributed to the presence of low-mass electrons in the material). The flexible photoconductive ribbon can be wound on a dielectric tubular support, to form the energy-magnifying coil 24.

In yet another example, a thick-film coating of photoconductive cadmium sulphide (CdS) or cadmium selenide (CdSe) is formed on a wire coil by sintering as paste, which comprises a powder of finely ground CdS or CdSe crystals mixed with water and at least a fluidiser such as cadmium chloride, at a temperature of 550° C. to 600° C. in a controlled atmosphere. During sintering, the boundaries of the small crystals become melted with the heated fluidiser, allowing the crystals to regrow together and solidify when the fluidiser evaporates and the sintered coating is cooled. Alternatively, copper oxides are formed in place on bare copper or bronze wire by heating the wire above about 260° C. in an oxygen atmosphere, or by application of chemical oxidants.

In yet another example, a coil of ceramic-like superconductor or photoconductor is made by tape-casting, extruding, slip-casting, cold or hot-pressing, or coating of the material as a thin film arranged helically on a tubular dielectric substrate. The assembly is heat-treated in a controlled atmosphere furnace to increase inter-crystalline contacts. Alternatively, the thin film of superconductor or photoconductor is formed over the entire exterior of the dielectric substrate, followed by removal of selected portions of the superconductor or photoconductor to form the desired helical coil.

[121]In some photoconductors and doped semiconductors, only a small portion of a population of inductive photons irradiated on the material, impact with, and yield acceleration of, low-mass electrons in the material. This is due to a low density of photoconductive low-mass electrons in the material. In such as case, inductive-photon radiation passing through the material can be captured efficiently by normal free conduction electrons in a metallic strip that desirably is in immediate contact with, or embedded in, the material. The acceleration of normal free electrons in the metallic conductor, sets up an electric field that assists in

accelerating the low-mass photoelectrons. In this configuration, it is desirable that the photoconductive material be disposed completely over and around the metallic strip so that the photoconductor faces both outwards and inwards, with both sides of the photoconductor or doped semiconductor being in electrical contact with each other.

One factor in the choice of photoconductor material to use in forming the energy-magnifying coil **24** is the potential magnification of energy that can be realised by low-mass electrons of an n-type or p-type photoconductive material. Other important factors are the quantity of low-mass electrons that are available in the photoconductive material for a given amount of illumination and the actual electrical conductance of the material. Standard illumination-sensitivity measurements provide a general overall index of the ability of a photoconductor to serve effectively in magnifying energy.

Cadmium sulphide and cadmium selenide, the most common photoconductive compounds which are available commercially, have calculated magnification factors of 37 and 59, respectively. The peak response wavelength of cadmium sulphide is 515 nanometers (in the green part of the visible spectrum) and of cadmium selenide is 730 nanometers (in the near-infrared part of the spectrum). Cadmium sulphide can be mixed with caesium selenide under certain conditions, so the resulting mixture assumes photoconductive characteristics between those two values. Mixtures can be produced having peak wavelengths which are matched to the wavelengths of commercially available LEDs of many sizes and illumination intensities. Some semiconductors which become photoconductive at a wavelength smaller than the wavelength produced by currently available LEDs can be made conductive of low-mass electrons merely by heating.

Applicant has found that gallium arsenide develops considerably higher conductivity than copper or silver at a temperature of 100⁰ C. and that the conductive electrons are low-mass. Also, alpha radiation is capable of liberating many low-mass electrons in some semiconductors. A second electron of comparatively low mass may have been liberated from cupric oxide by alpha radiation along with the outer copper electron in Leimer's (1915) experiments, since the measured energy magnification exceeded the magnification calculated from cyclotron resonance of CuO, which most likely pertains only to the mass of the outer electron.

Dopants can be added to a semiconductor to make it more conductive of low-mass electrons without illumination. Also, the illumination-sensitivity and conductivity of cadmium sulphide are increased by adding small amounts of donor-type dopants such as, but not limited to, sulphides, selenides, tellurides, arsenides, antimonides and phosphides of the Type-IIIa elements: aluminium, gallium, indium and thallium. In this regard, the photoconductors of high-sensitivity photovoltaic cells may comprise as many as five different compounds. The actual mixtures of photoconductive compounds and dopants used in commercially available photovoltaic cells often are trade secrets. But, the sensitivity and conductances of the cells are usually given or are measurable, and these data can be used advantageously in selecting a particular photoconductive compound for use in the apparatus.

Other photoconductive compounds or elements can be employed in energy-magnifying coils. For example, the conduction electrons of silicon have an energy-magnification factor of 15 times. Photoconductors having very high magnification factors include, but are not limited to, gallium arsenide, indium phosphide, gallium antimonide, cadmium-tin arsenide, and cadmium arsenide, which have calculated energy-magnification factors ranging between 200 times and 500 times, and mercury selenide (1100 times), indium arsenide (2000 times), mercury telluride (3400 times) and indium antimonide (5100 times).

The depth of optical transmission largely determines the optimum thickness of photoconductive films for energy-magnifying coils. For example, the highest optical transmission of sintered CdS is reported to be 20 micrometers, but since the average grain size increases (and the average porosity decreases) with an increase in film thickness, the maximum conductivity of a sintered film is at a thickness of 35 micrometers (J. S, Lee et al., 1987).

The metal chosen to be embedded must not react chemically with the photoconductor. For example, aluminium reacts with gallium arsenide (GaAs) in an electrical environment, to change the conductive character of both the GaAs and the aluminium. Gold, platinum, and palladium can serve in many cases because these materials are relatively inert chemically. Gold combines chemically with tellurium, however, so gold is not suitable for embedding in mercury telluride. Cadmium plating over a common metal serves to alleviate the reactivity in cases where cadmium sulphide or cadmium selenide is used as the photoconductor.



The discussion above has been, for ease of explanation, in the context of the apparatus including one energy-magnifying coil 24. However, as discussed, use of a single energy-magnifying coil 24 to capture inductive photons from the sending coil 20, results in loss (by non-capture) of most of the inductive photons from the sending coil 20. This proportion of captured inductive photons can be increased greatly in an embodiment in which multiple energy-magnifying coils 24 substantially completely surround the sending coil 20, such as shown in Fig.4. In this embodiment, the energy-magnifying coils 24 substantially completely surround the sending coil 20, and (although six energy-magnifying coils 24 are shown) as few as three energy-magnifying coils 24 of adequate diameter, still could substantially completely surround the sending coil 20. There is no limit, except as possibly related to packaging concerns, to the maximum number of energy-magnifying coils 24 which could be used. The depicted configuration of Fig.4, has a desirable number of six energy-magnifying coils 24. In Fig.4, the shaded sectors 31, considered collectively, illustrate that nearly all 360 degrees of inductive-photon radiation 22 from the sending coil 20, are received by the energy-magnifying coils 24. Not shown in Fig.4 are photoconduction exciters (items 26 in Fig.3) used for illuminating respective portions of the energy-magnifying coils 24 in a photoconductive form of the apparatus 15.



Fig.4 also depicts respective internal output coils **28a** nested co-axially and co-extensively inside each of the energy-magnifying coils **24**. As discussed earlier, each internal output coil **28a** receives nearly all the inductive-photon radiation propagating radially inwards from the respective energy-magnifying coil **24**. Desirably, the overall energy output of the embodiment of **Fig.4**, can be increased by surrounding the array of energy-magnifying coils **24** with an external output coil **28b**, of which the conductors desirably are made of insulated metallic wire (**Fig.5**). In this embodiment, approximately half of the outwardly propagating magnified inductive-photon radiation (large arrows **18**) from each energy-magnifying coil **24** (one such coil is highlighted in **Fig.5**) is received by the external output coil **28b**. This captured radiation is denoted by the shaded sector **35**. When this externally directed inductive radiation captured from all the energy-magnifying

coils **24** is added to all the inwardly directed radiation captured from the energy-magnifying coils **24** by their internal output coils **28a**, **28b**, greatly exceeds the back-force energy directed by the energy-magnifying coils **24** towards the sending coil **20** (the back-force energy from one energy-magnifying coil **24** is shown as the shaded sector **16**). Thus, the resulting energy "leverage" exhibited by the apparatus is increased substantially by including the external output coil **28b**.

The embodiment of **Fig.5** also includes respective arrays (viewed endwise) of light-emitting diodes (LEDs) collectively serving as photoconductor exciters **26** for the energy-magnifying coils **24**. The LED arrays are arranged back-to-back and disposed between adjacent energy-magnifying coils **24**. Each array in **Fig.5** can comprise multiple LEDs or as few as one LED.



Fig.6 provides a perspective view of an apparatus 15 having an arrangement of coils similar to the arrangement shown in Fig.5. In Fig.6, each energy-magnifying coil 24 comprises a helical coil of superconductive or photoconductive material in wire or ribbon (tape-like) form.

Whenever multiple energy-magnifying coils **24** are used, the respective directions of electron flow in them desirably occur in the same circular direction as viewed endwise. Thus, the flow of electrons in all the energy-magnifying coils **24** is clockwise during one phase of an oscillation cycle and counterclockwise during the other phase. The same principle applies to the flow of electrons in the output coils **28a**, **28b**. (But, in such an embodiment, the flow of electrons in the output coils **28a**, **28b**, is in the opposite direction to the electron flow in the energy-magnifying coils **24**). These relationships of electron flow in the coils during a particular phase of an oscillation cycle, are shown in **Fig.7**.

The energy-magnifying coils 24 desirably are connected together in series, using inter-coil connectors 30a. 30b, to maintain the same direction of electron flow, which can be clockwise or counterclockwise (as viewed from one end of such a coil). This direction of electron flow in a coil is termed the "handedness" of the coil. If the energy-magnifying coils 24 all have the same handedness, then the ends of adjacent energymagnifying coils 24 are connected together in a head-to-foot manner progressively in one direction around the group of coils (not shown). ("Head" refers to the forward-facing end, and "foot" refers to the rearwardfacing end of the apparatus in relation to the viewer). In this case, the inter-coil connectors **30a**, **30b**, must pass either completely through the apparatus or around the outside of the apparatus for its entire length, which reduces efficiency and can cause undesirable wear if the connectors are subjected to vibrations. A more desirable arrangement is depicted in Fig.6, in which short inter-coil connectors 30a, cross directly head-to-head between one energy-magnifying coil 24 and an adjacent energy-magnifying coil 24, and short inter-coil connectors 30b cross over directly foot-to-foot in the next energy-magnifying coils 24. In this configuration, the handedness of turns of the energy-magnifying coils 24 alternates from right-to-left to leftto-right in adjacent energy-magnifying coils 24. In the same manner as a right-handed screw advances from head to foot as it is turned clockwise, and a left-handed screw moves in the opposite direction, clockwise electron flow in a right-handed coil advances from head to foot, and clockwise electron flow in a left-handed coil advances from foot to head.

The single-layered internal output coils **28a** in **Fig.6**, present the same situation in which these coils are connected in series. Desirably, the inter-coil connectors **32a** cross over directly from one internal output coil

28a to the adjacent internal output coil 28a, head-to-head and the inter-coil connectors 32b cross over directly foot-to-foot from one internal output coil 28a to the adjacent internal output coil 28a. This same handedness convention generally applies to all series-connected internal output coils 28a connected in this manner. The head-to-head inter-coil connectors 32a and foot-to-foot inter-coil connectors 32b for the internal output coils 28a, need not coincide with the same respective connectors 30a, 30b for the energy-magnifying coils 24.

In another embodiment (not shown), each internal output coil is two-layered, with both leads at either the head or foot. Such a configuration allows for short and direct connections between adjacent internal output coils. Multiple-layered internal output coils may be more efficient, but the extra layers of coiled wire increase the mass of the apparatus, which may be a concern in mobile applications. Multiple wire layers carrying high current may also result in overheating, which may require that some space be left between each internal output coil **28a** and its surrounding energy-magnifying coil **24** to accommodate one or more conduits of a coolant through the apparatus (at a sacrifice of some efficiency). The coolant can be, for example, forced air (in the case of photoconductors or doped semiconductors) or liquefied cryogenic gas (in the case of superconductors).

Fig.6 also shows two external conductors **34** connected to respective internal output coils **28a**. Electrons flow through the conductors **34** and the internal output coils **28a** in series. In addition, two external conductors **36** are connected to respective ends of the external output coil **28b**, and two external conductors **38** are connected to respective ends of the sending coil **20**.



Fig.7 is a schematic end view of the apparatus of **Fig.6**, showing the relative direction of electron flow in the various coils and in the inter-coil connections described for single-layer coils. At a particular oscillation phase, the clockwise electron flow denoted by the arrow **39a** in the sending coil **20** induces clockwise electron flow **39b** in all the energy-magnifying coils **24**. The magnified radiation from the clockwise electron flow in the energy-magnifying coils **24**, induces counterclockwise electron flow in all the internal output coils **28a**, as indicated by the arrows **39c**. The counterclockwise electron flow, denoted by the arrow **39d**, in the external output coil **28b** is opposite in direction to the electron flow in the energy-magnifying coils **24**.

The electron flow in the inter-coil connectors **30a** extending between adjacent energy-magnifying coils **24** is indicated by the arrows **39e**, and the electron flow in the inter-coil connectors **32a** extending between adjacent internal output coils **28a** is indicated by the arrows **39f**. During the next oscillation phase, all the direction arrows shown in **Fig.7** reverse themselves.

Connecting the internal output coils **28a** together in series is advantages if it is desired to maximise the output voltage from the apparatus **15**. Alternatively, the internal output coils **28a** can be connected together in parallel if it is desired to maximise the output electrical current from the apparatus **15** while minimising the output voltage. In this alternative configuration, all the internal output coils **28a** desirably are wound with the same handedness, with each coil **28a** having two respective leads. The leads at one end (e.g., the foot end)

of the coils **28a** are connected to each other, and the leads at the other end (the head end) of the coils **28a** are connected to each other. The resulting parallel-coil system is connected in a conventional manner in other circuitry of the apparatus (not shown).

Further alternatively, the internal output coils **28a** can be connected together so as to provide more than one output circuit (so long as sufficient energy is produced for use as feedback to the sending coil **20** and for use in establishing favourable conditions for producing abundant low-mass electrons). Alternatively, the relative voltage(s) and current(s) of output power can be varied by changing the ratio of the number of turns in the energy-magnifying coils **24** to the number of turns in the internal output coils **28a**. Alternatively again, the energy-magnifying coils **24** can be employed in a separate manner to provide more than one energy-magnifying unit. Each unit can comprise one or more energy-magnifying coils that can serve its respective circuit of internal output coils.

The two conductors **36** connected to the external output coil **28b**, can be connected to the internal output coils **28a** or can be used (without being connected to the internal output coils **28a**) with only the external output coil **28b** to provide an independent output circuit (not shown). The two conductors **38** connected to the sending coil **20**, are connected in the feed-back loop **46** such that electron flow in the sending coil **20** is in the same circular direction as in the internal output coils **28a**.



Fig.8 depicts yet another embodiment of the apparatus 15, in which each energy magnifying coil 24 comprises a thin film or thick film of a polycrystalline or other suitable photoconductor deposited in a helical manner directly on to a tubular substrate 40 desirably made of ceramic or other suitable dielectric material. on each energy magnifying coil 24, the polycrystalline photoconductor is formed as a helical band on the outside of the tubular substrate 40. The helical band of photoconductor can include a thin film of metal embedded within it. In certain cases, inter-coil connections between adjacent energy magnifying coils 24 can be made by extending the deposited photoconductor from the helices to contact areas 44 situated at the ends of the tubular substrates 40 and extending toward contact areas 44 on adjacent tubular substrates 40. Electrical contact between adjacent energy magnifying coils 24 is made under moderate pressure via the contact areas 44, which are shown in Fig.8. To distinguish the individual contact areas 44, they are shown in a separated position before being pressed together to make contact. To maintain the integrity of the contact areas 44, the energy magnifying coils 24 can be held together in mutual proximity by any of various non-metallic fasteners to make continuous electrical contact between all of the photoconductive portions. For example, bolts 43 and nuts 45 made of a plastic such as nylon, or other dielectric material, can be used. Another variation is to maintain contact pressure of one coil to the next by means of spring clips. Thus, in one embodiment, the energy magnifying coils 24 are connected so as to be in endless contact with each other, with no capacitative break between them. The remainder of the apparatus can be constructed in the same manner as the photoconductor or doped-semiconductor embodiment described above, wherein the same attention to the direction of electron flow in respective coils is observed.



The coil configuration of yet another embodiment is shown in **Fig.9A** and **Fig.9B**. A tubular substrate **40**, supports a helical, thin film or thick film, dipole-type of energy-magnifying coil **24** that is nested inside and coaxial with a single external output coil **28b**. Nested inside the tubular substrate **40**, and with respective axes parallel to the axis of the tubular substrate **40**, are a sending coil **20** and an internal output coil **28a**. The sending coil **20** and the internal output coil **28a**, are positioned on opposite sides of a reflective metallic separator **59**. The separator **59** is substantially parabolic in cross-section throughout its axial extent, and is positioned so that the longitudinal edges are touching, or nearly touching, the tubular substrate **40**. The sending coil **20** is positioned on the concave side of the separator **59**, with the axis of the sending coil **20** being positioned at the geometric focus **60** of the parabola and disposed parallel to the axis of the energy-magnifying coil **24**. The energy-magnifying coil **24** in this embodiment, comprises a thin film or thick film photoconductor formed helically on the tubular substrate **40**. A photoconduction exciter **26** is positioned inside the separator **59**. (The tubular substrate **40**, is made of a rigid material that is transparent to radiation produced by the photoconduction exciter **26**). All the other forms of the energy-magnifying coil **24** as described herein, including the superconducting form, can be employed in this embodiment.

The separator **59**, serves a double purpose. One purpose is to direct towards the energy-magnifying coil **24** the portion of the inductive-photon radiation **22** which is not otherwise directed towards the separator, as shown by the reflected-photon rays **61** in **Fig.6A**. (Reflection of these radiated photons does not change the directionality of the transverse force which these photons convey). Another purpose of the separator **59** is to serve as a shield to restrict the amount of inward radiation **18b** from the energy-magnifying coil **24** which is returned as a back-force to the sending coil **20**. The restricted back-force radiation is shown by the shaded area **63** in **Fig.9B**.



The portion of the inwardly directed, magnified inductive-photon radiation **18b** which is received by the internal output coil **28a**, is denoted by the shaded area **65**. The proportional amount of outwardly directed magnified radiation **18a** from the energy-magnifying coil **24** which is received by the external output coil **28b**, is shown by the shaded area **67**. The sum of the magnified radiation in the area **65** which reaches the external output coil **28b**, substantially exceeds the magnified radiation in the area **63** (the latter serving as a back-force on the sending coil **20**). This excess of utilised energy over the back-force energy, provides energy leverage. This embodiment also includes a starting mechanism, and initial power source for the photoconduction exciter, a work loop, and a feedback loop (not shown) as provided in the other embodiments described herein.



Certain features can be incorporated with any of the embodiments described herein, to add functional practicality. For example, referring to the schematic representation of a coil configuration shown in end view

in **Fig.10A**, a ferromagnetic core **69** can be placed inside the sending coil **20**, and ferromagnetic cores **71** can be placed inside respective internal output coils **28a**. These cores increase the inductance of the apparatus, which lowers the frequency of the electrical oscillations produced by the apparatus. Although increases in inductance can cause the output voltage and current to be out of phase, the phase difference can be corrected by adding capacitance to the circuitry by conventional means. Also shown, is an external metal shield which completely surrounds the apparatus to block any radiation from the device that could interfere with radios, televisions, telephones, computers and other electronic devices. the shield can be comprised of any of various non-magnetic metals such as aluminium or magnesium.

An alternative means of increasing the inductance of the apparatus is shown in **Fig.10B**, which is a variation of the end view of just the sending coil **20** that is depicted in **Fig.10A**. In **Fig.10B**, a ferromagnetic sleeve **73** is placed coaxially around the sending coil **20**.

The respective dimensional ratios of various components generally remain similar with respect to each other for different apparatus sizes, except for the longitudinal dimension, which generally can be as short or as long as desired, up to some practical limit. The respective gauges of wires used in the sending coil **20** and the output coils **28a** and **28b**, are commensurate with the electric current carried by these wires, and the respective thickness of insulation (if used) on the wires is commensurate with the voltage.

The outside diameter of the internal output coils **28a** desirably is only slightly less than the inside diameter of the respective energy-magnifying coils **24**, as shown in **Fig.6**, **Fig.7** and **Fig.8**, thereby ensuring close proximity of each internal output coil **28a** with its respective energy-magnifying coil **24**. At a sacrifice in efficiency, the outside diameter of the internal output coils **28a** can be made smaller, to allow space for heat from the current-carrying wires to escape or be removed by a coolant such as forced air in the case of a photoconductor type or doped semiconductor type apparatus, or by a cryogenic liquefied gas in the case of a superconductor type apparatus.

Also, desirably, the external output coil **28b** is connected in series with the internal output coils **28a** to maximise the output voltage from the apparatus **15** and to minimise heat produced by electric currents in the apparatus. The output voltage can be stepped down and the output electric current stepped up to normal operating ranges by using a transformer, wherein the primary of the transformer would comprise the load in the work loop **48**.

As discussed above, each energy-magnifying coil **24** can comprise a photoconductor or doped semiconductor formed as a helical pattern on a respective thin-walled tubular substrate provided with extended, raised contact surfaces at each end. The energy-magnifying coils **24** desirably are connected electrically (rather than capacitatively) to each other in series at the raised contact surfaces. The photoconductive coils desirably are coated using clear varnish or enamel to provide electrical insulation and to protect the photoconductors from oxidation and weathering.

Where the low-mass photoconducting electrons in the energy-magnifying coils **24** are present in a concentration which is insufficient for capturing most of the inductive-photon radiation from the sending coil **20**, each energy-magnifying coil desirably includes a thin metallic band. The metal desirably is in intimate contact with the low-mass-electron carrier. the metal can be on the exterior of a doped semiconductor, or it can be embedded in a photoconductor band of the coil to capture the inductive radiation and set up an electric field which, in turn, assists in accelerating the low-mass electrons. In the photoconductive material desirably is disposed all around the metallic band so that the low-mass electrons are conducted on the outer side as well as the inner side and edges of the photoconductive band on the portion or portions which are exposed to illumination on the outside. The width of the metal band desirably is sufficient to capture as much of the inductive-photon radiation from the sending coil as is practical, since gaps between turns of the metal band in the energy-magnifying coil permit the sending coil's inductive radiation to pass through to the internal output coil. Since the sending coil's radiation is a half-cycle out of phase with the inductive radiation from the low-mass electrons, all the sending coil radiation which reaches the output coil, reduces the output efficiency of the apparatus.

Appropriate photoconductive materials (e.g. cadmium sulphide, cadmium selenide) for forming the energymagnifying coils **24** are commercially available. The photoconductive material can be a single material or a mixture of materials, and can be formed by, for example, sputtering. A mixture of cadmium sulphide and cadmium selenide can be adjusted optimally to yield energy-magnifying coils exhibiting maximal energymagnifying factors at a peak wavelength matching the brightest photoconduction exciters **26** which are available. With respect to the photoconduction exciters **26**, photo-excitation of the energy-magnifying coils **24** can be provided by one or more LEDs, either surface-emitting or edge-emitting, for example, selected to produce an output wavelength matched to the peak photoconduction wavelength of the energy-magnifying coils **24**. In the embodiment of **Fig.7** and **Fig.10A**, individual LEDs **26** are positioned in linear arrays mounted back-to-back on respective mounting bars. The assembled mounting bars with LEDs are placed in the gaps between adjacent energy-magnifying coils **24** to illuminate at least the sides of the respective energy-magnifying coils **24** which receive inductive-photon radiation from the sending coil **20**. LEDs are advantageous compared to incandescent lamps because LEDs produce more light with less heat and have a much longer operational lifetime than incandescent lamps. LEDs are also preferred because of their small size which facilitates fitting a large number of them into the relatively small space between adjacent energy-magnifying coils **24**.

Whereas the invention has been described in connection with several representative embodiments, the invention is not limited to those embodiments. On the contrary, the invention is intended to encompass all modifications, alternatives and equivalents as may be included within the spirit and scope of the invention, as defined by the appended claims.

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